

# High Strength Forged Steel and Process Design

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Metallurgy for Forging Process Design and Tool Life Improvement vs. XRD Forum

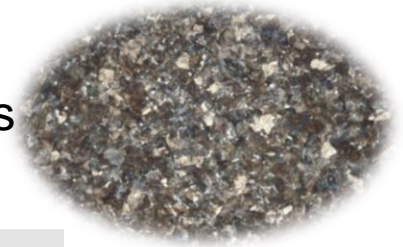
Wed 29 January 2020

# Outline



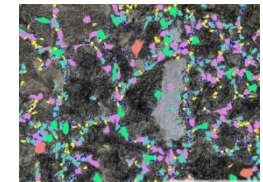
## State of the Art

- Products from Microalloyed Forged Bars
- Microstructure of Air-Cooled Microalloyed Forged Steels
- Strength of Steel and Strengthening Mechanisms



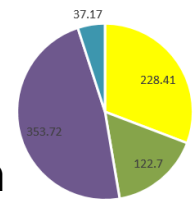
## 2 Method

- Industry-near Forging Experiment
- Metallography: LOM for phase fraction and grain size
- Mechanical Properties: tensile testing, hardness, impact
- Fraction of Precipitates: Synchrotron XAS



## 3 Results and Discussion

- Cooling Curves with Recalescence
- Calculated Contribution from each Strengthening Mechanism



# Microalloyed Forged Steels

## Typical Applications in Automotive Industry

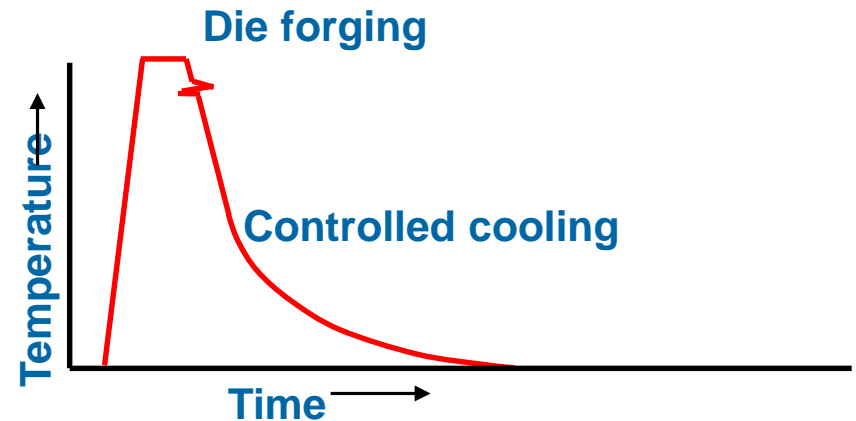
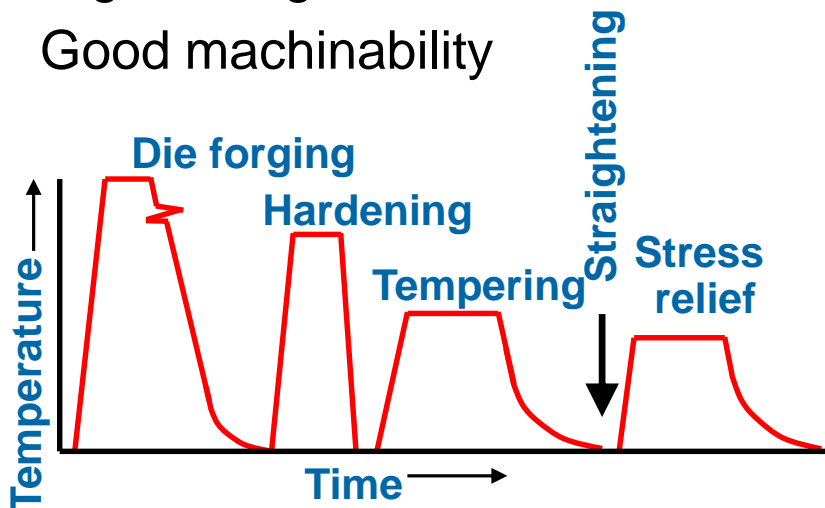
- Crankshaft
- Connecting rod
- Steering link
- Axle leg
- Wheel carrier
- Control arm
- Piston for diesel engines
- Common rail for diesel engines



• **Source:** Basic Knowledge Forgings – Significance, Design, Production, Application, Industrieverband Massivumformung

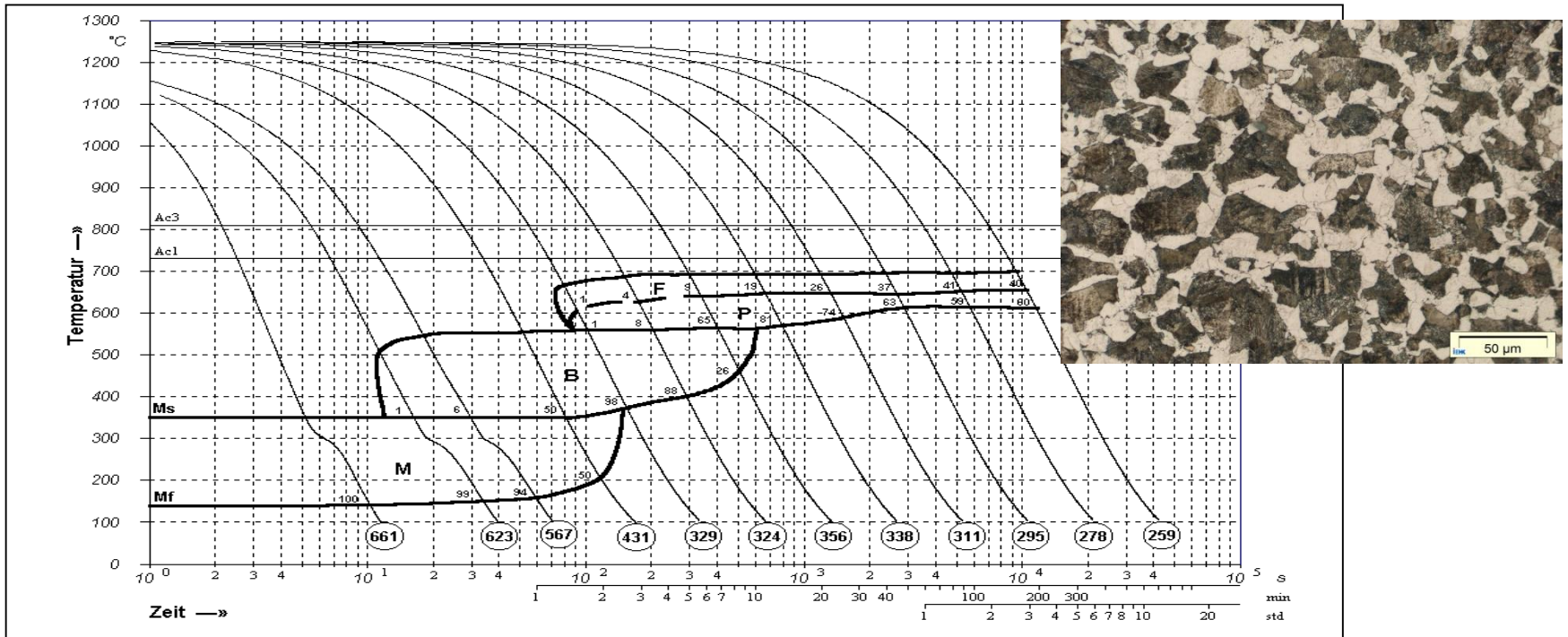
# Microalloyed Forged Steels

- Quenched and tempered steel (Q&T) needs an additional heat treatment (left picture)
- Microalloyed steels achieve final properties during controlled cooling directly after forging (right picture)
- Shorter process chain compared to Q&T steels → No costs for additional heat treatment
- No risk for crack formation during quenching
- Low cost alloying concept
- High strength
- Good machinability



# Microalloyed Forged Steels

## 38MnVS6 as an example for a typical steel and its transformation behavior

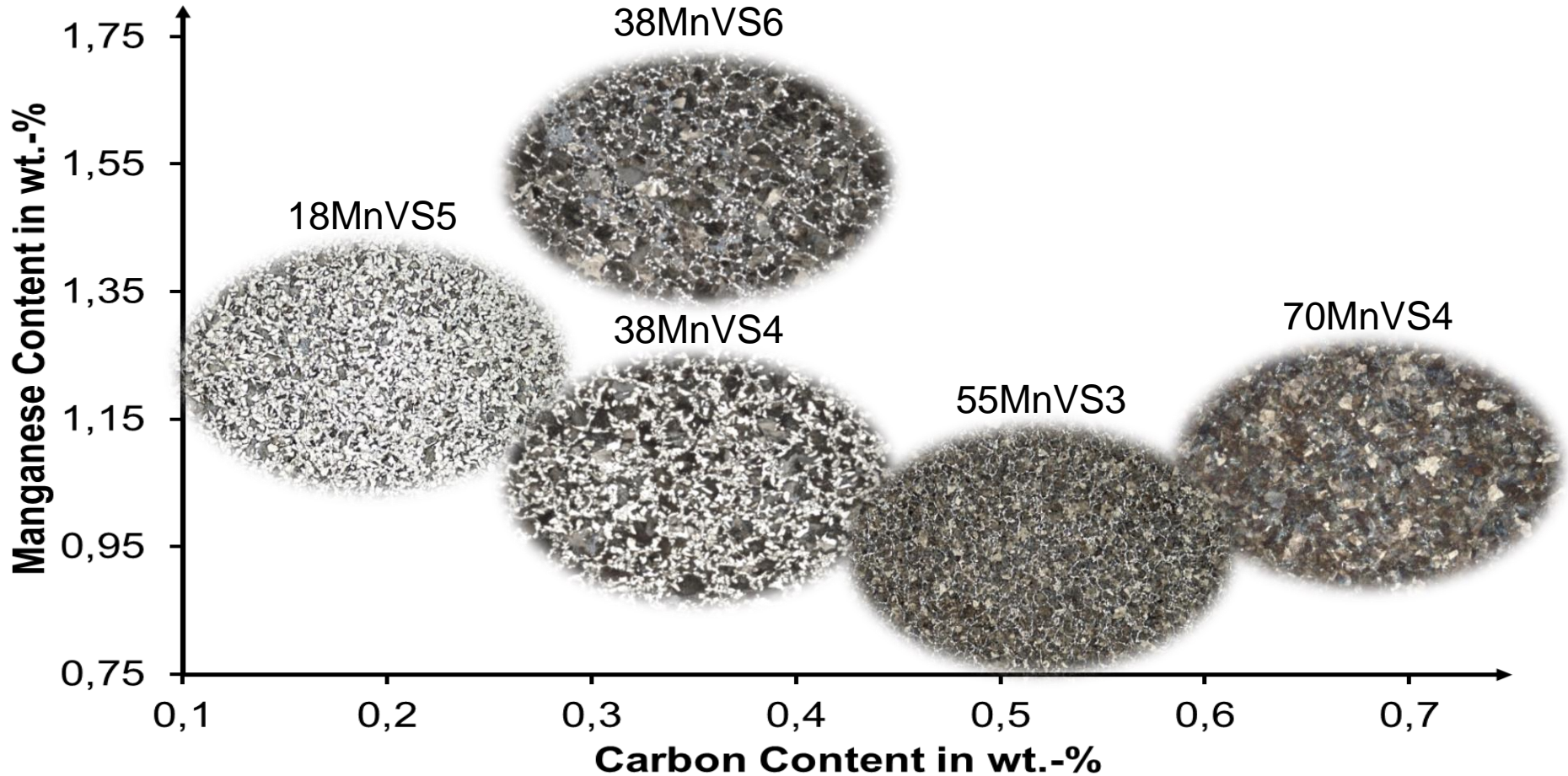


Chemical

Composition in wt.-%

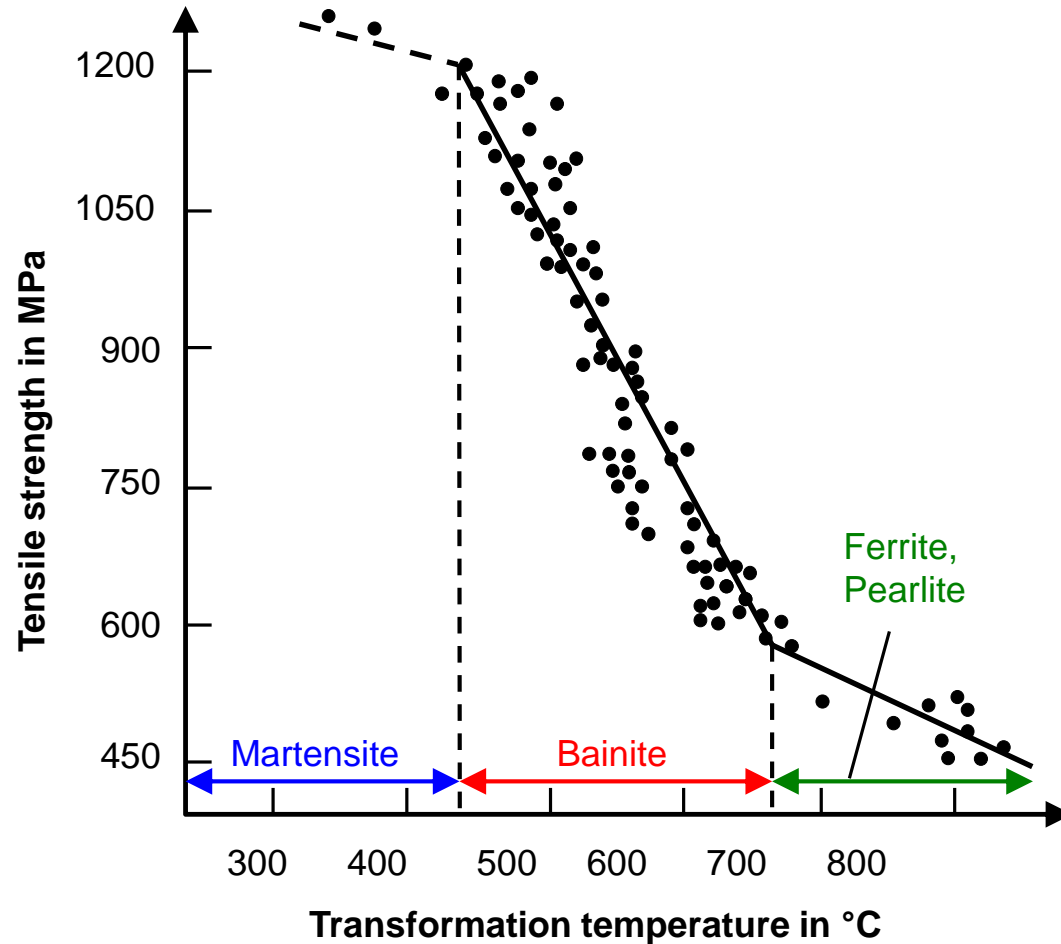
C	Si	Mn	P	S	Cr	Al	V	N
0,38	0,58	1,39	0,016	0,056	0,16	0,048	0,11	0,017

# Microalloyed Forged Steels - Adjusting Phase Fractions



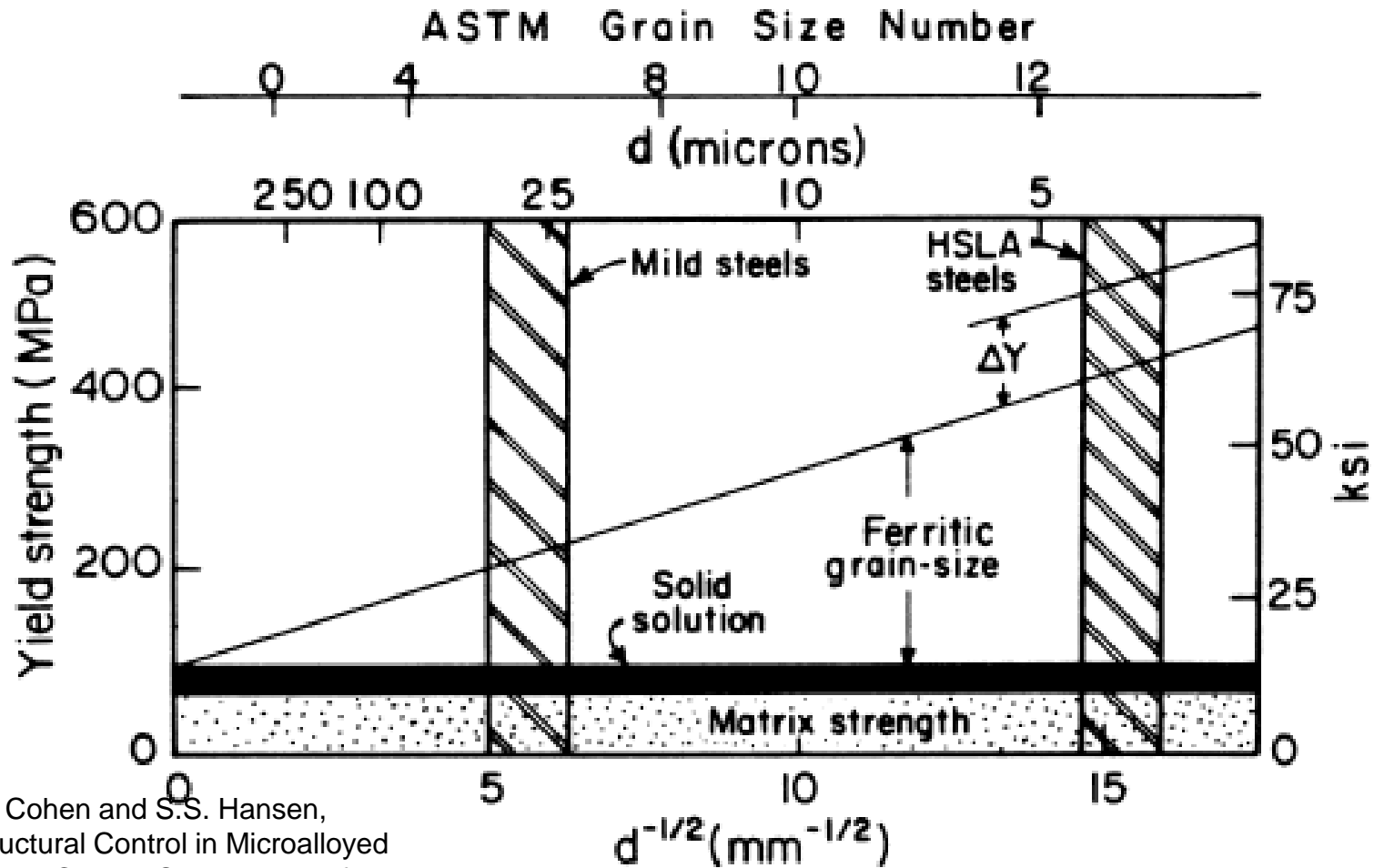
Source: H. Dickert et al, Steels in Cars and Trucks 2017

# Strength of Different Matrices according to Pickering



Ref.: F.B. Pickering, in Transformation and Hardenability in Steels, Climax Molybdenum Co., Ann Arbor, Michigan, 1967, p. 109.

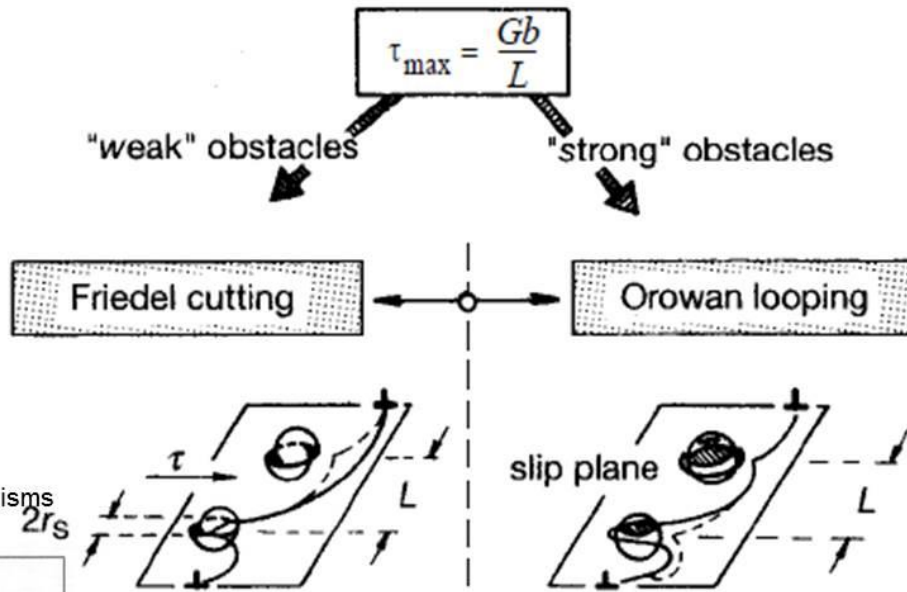
# Contribution to Yield Strength in Mild and HSLA Steels



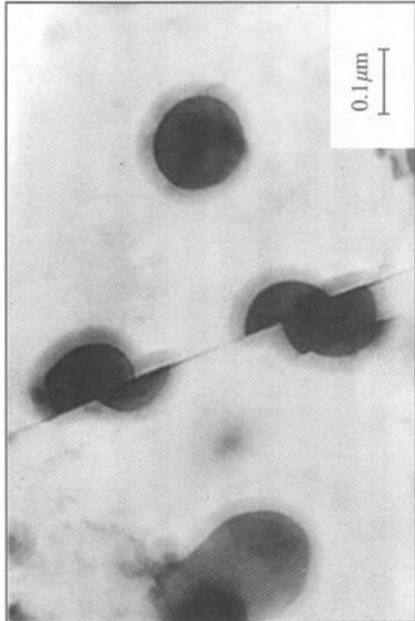
Ref. :M. Cohen and S.S. Hansen, Microstructural Control in Microalloyed Steels, in MiCon78: Optimization of Processing, Properties, and Service Performance Through Microstructural Control, ASTM STP 672, H. Abrams, G.N. Maniar, D.A. Nail and H.D. Solomon, Ed., 1979, p 34-52



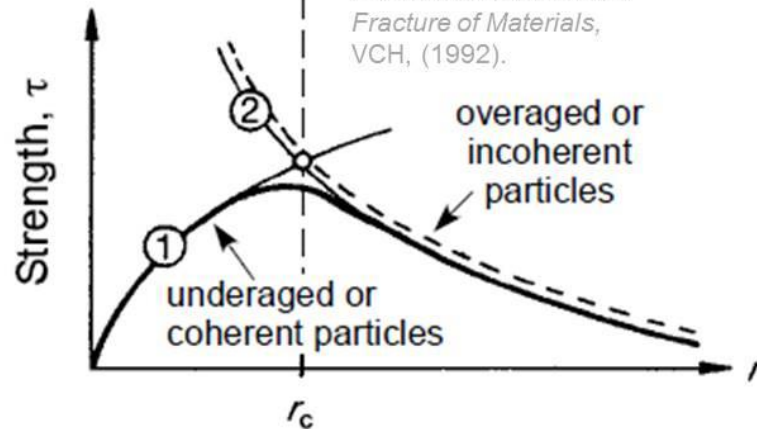
# Precipitation Hardening: Cutting vs. Looping



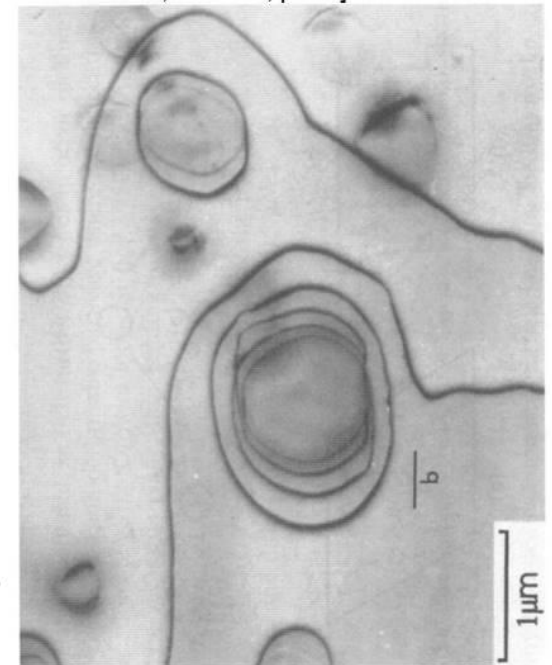
Argon, Strengthening Mechanisms in Crystal Plasticity., p.221



Adapted from Reppich, in *Plastic Deformation and Fracture of Materials*, VCH, (1992).



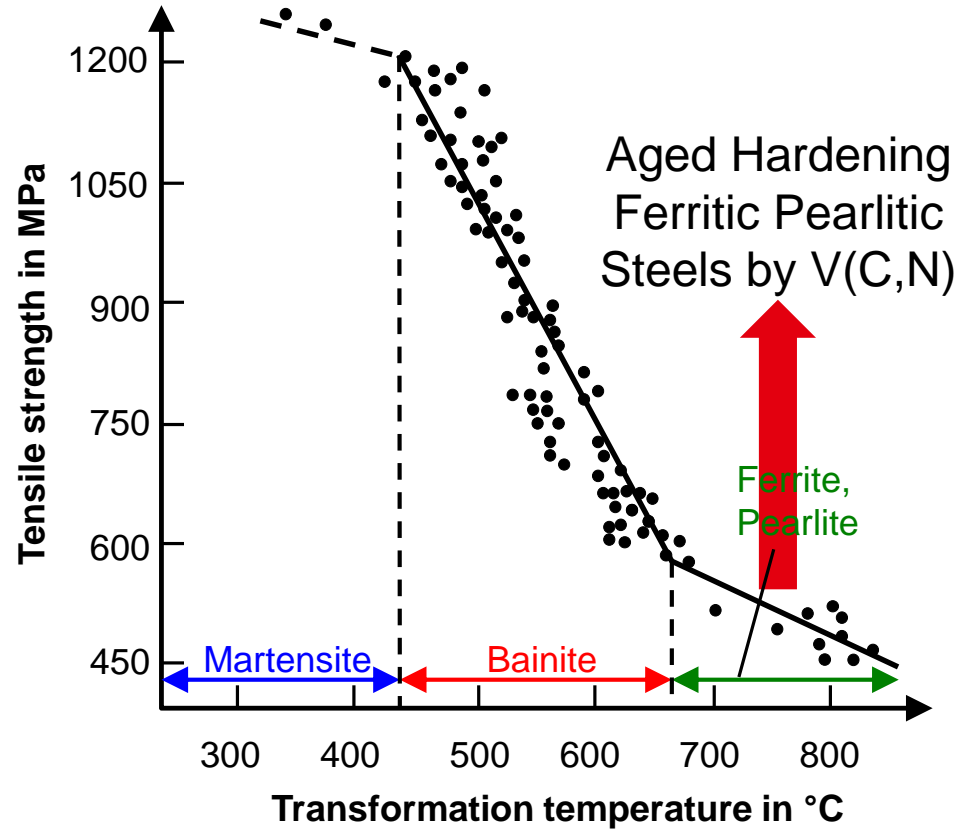
Ref.: Humphreys and Hatherly, *Recrystallization and Related Annealing Phenomena*, 2nd Ed., p.49.]



# Precipitation Hardening in Ferrite-Pearlite

$$\begin{aligned}
 YS &= f_{\alpha} \{ 35 + 58(\%Mn) + 17.4(D_{\alpha})^{-0.5} \} \\
 &+ (1 - f_{\alpha}) \{ 178 + 3.8(\lambda_p)^{-0.5} \} \\
 &+ 63(\%Si) + 425(\%N)^{-0.5} + \Delta YS_p
 \end{aligned}$$

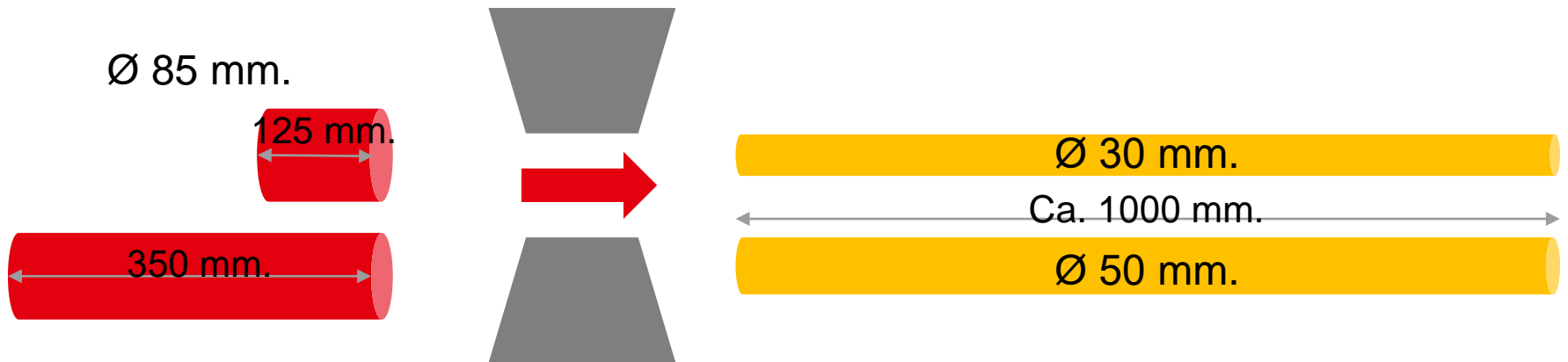
$\Delta YS_{p,Orowan-Ashby}$



S. Zajac, T. Siwecki, W.B. Hutchinson and R. Lagneborg: Strengthening Mechanisms in Vanadium Microalloyed Steels Intended for Long Products, ISIJ international 38.10 (1998), pp. 1130-1139

# Method: Industrial Cast and Forging Experiments

C	Si	Mn	P	S	Cu	Al	Cr	Mo	Ni	N	V	Ti
0.37	0.59	1.05	0.013	0.025	0.11	0.016	0.17	0.04	0.11	0.013	0.268	0.018



# Industrial Process

- Final Cooling on the conveyor belt is controlled by:
  - Speed of the conveyor belt
  - Use of fans (to increase cooling rate)
  - Covering the conveyor belt (to reduce the cooling rate).



# Method: Industry-near Process

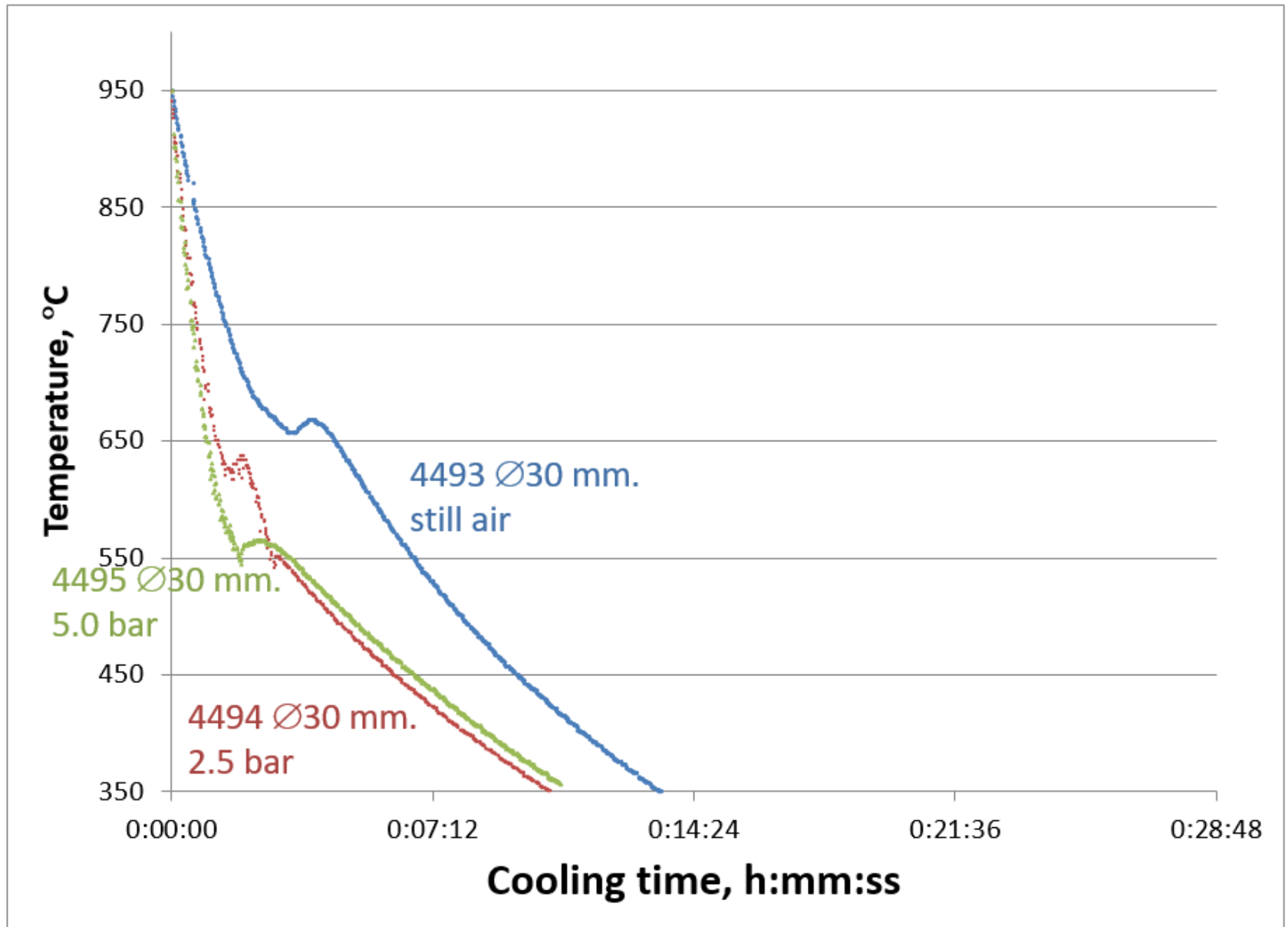
- Open die manual forging on a forging hammer
- Controlled cooling by using different pressures of compressed air
- Temperature measurement with a pyrometer



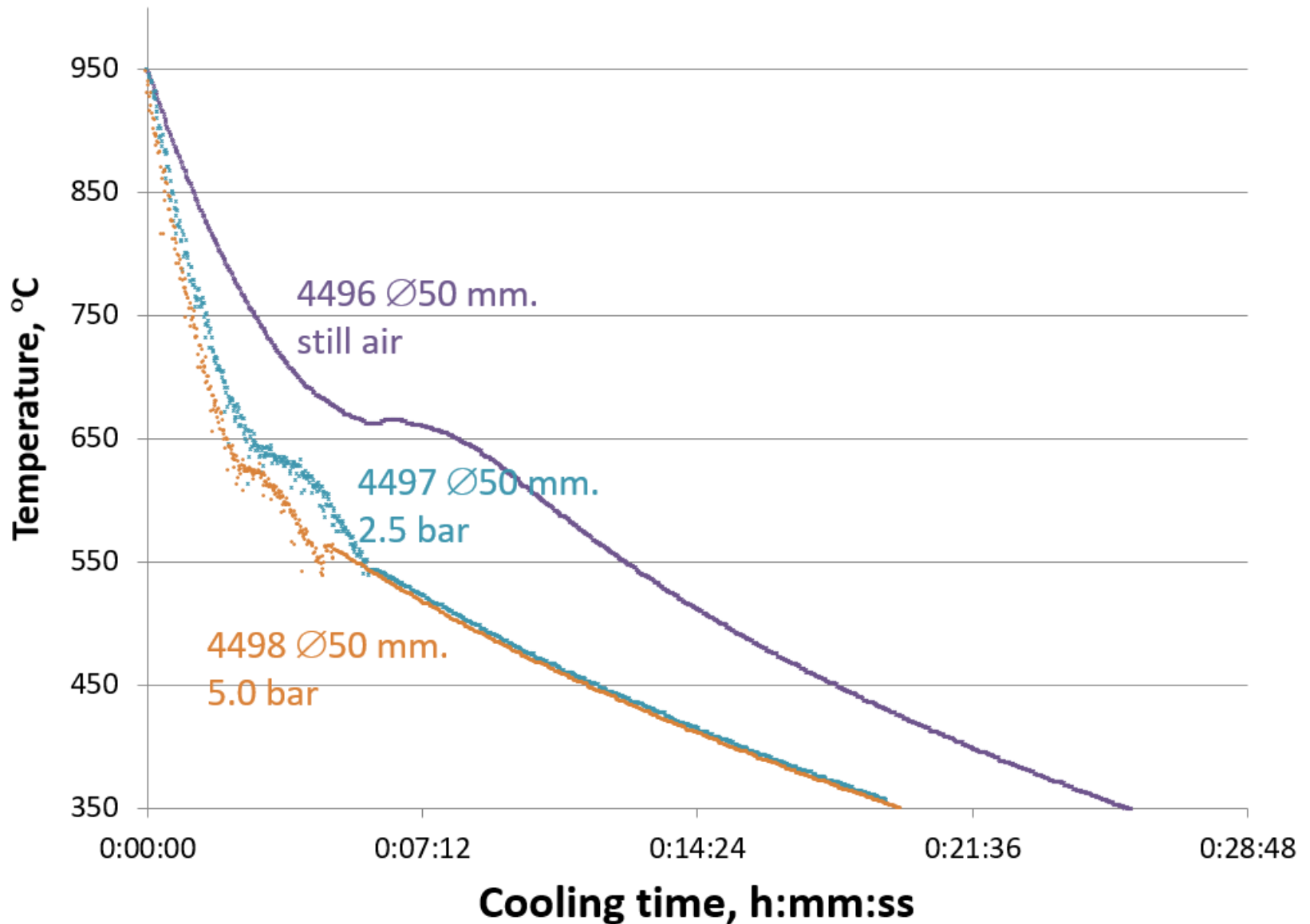
**CONFIDENTIAL**



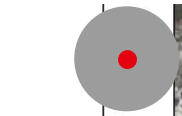
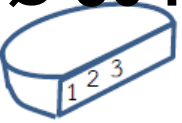
# Results: Cooling Curves with Recalescence



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Ø 30 mm.



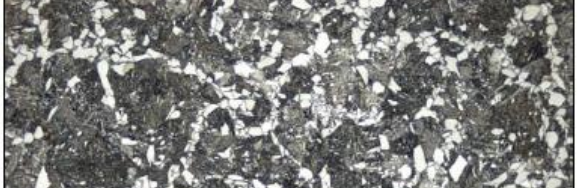
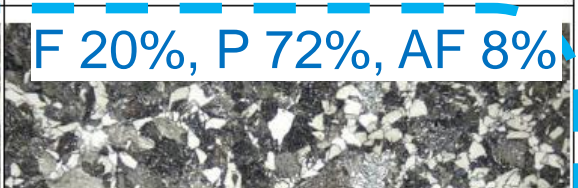
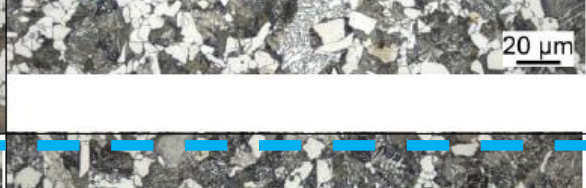
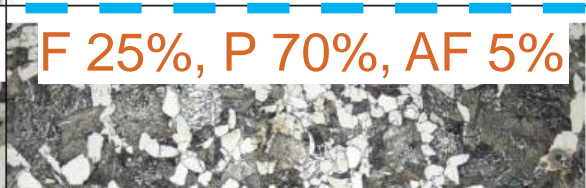
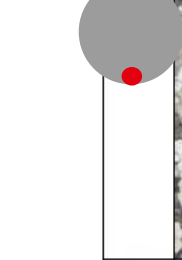
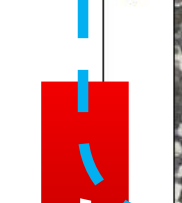
F 35%, P 65%,



F 25%, P 70%, AF 5%

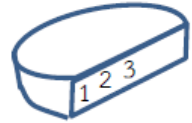


F 20%, P 72%, AF 8%





Ø 50 mm.



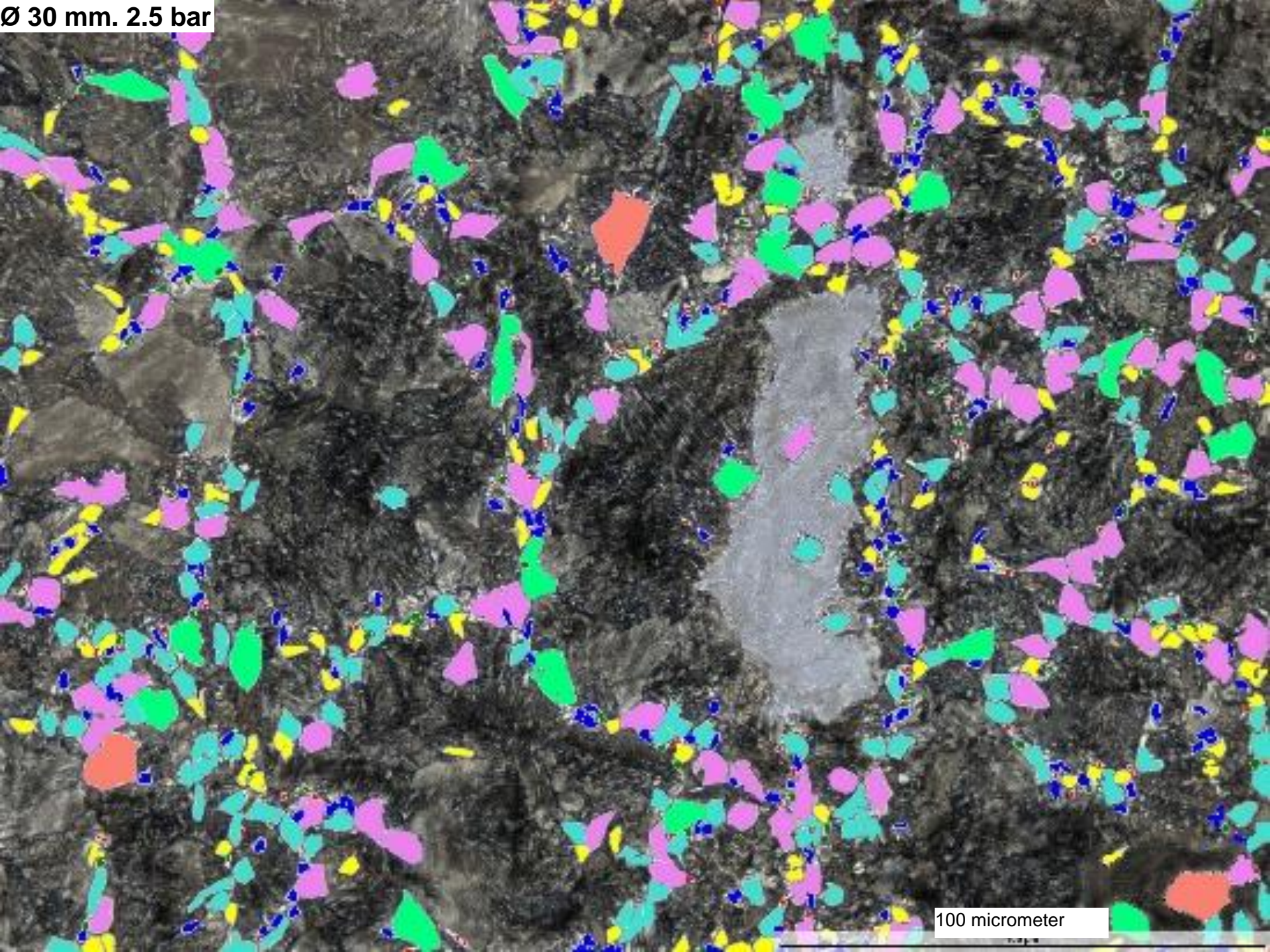
F 35%, P 65%,

F 30%, P 67%, AF 3%

F 25%, P 70%, AF 5%

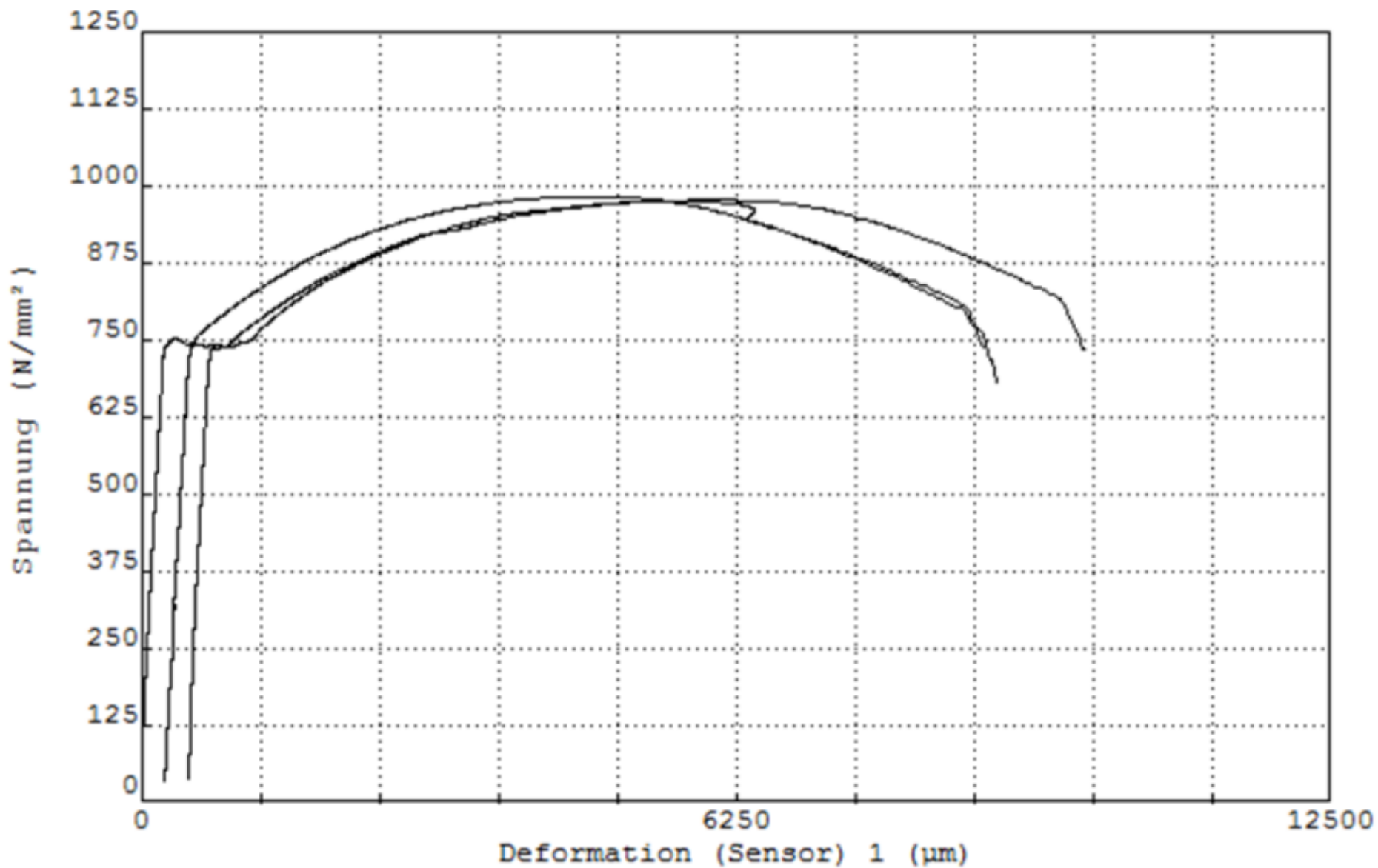


Ø 30 mm. 2.5 bar

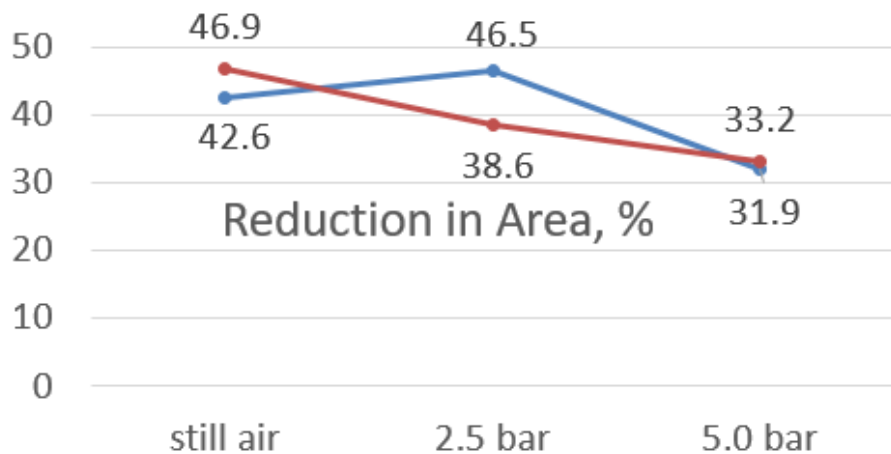
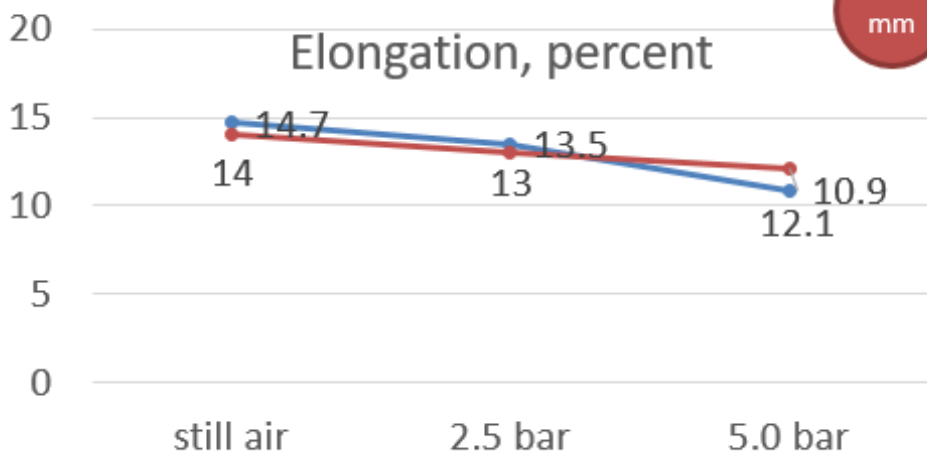
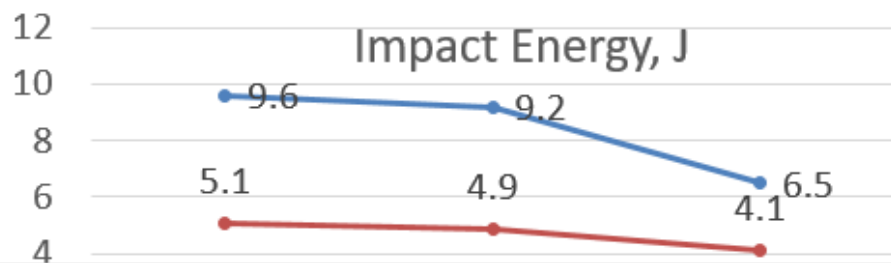
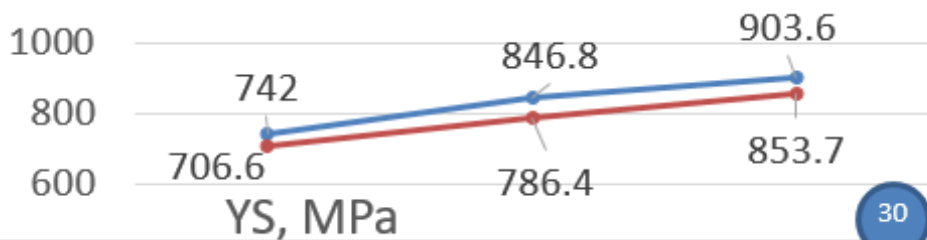
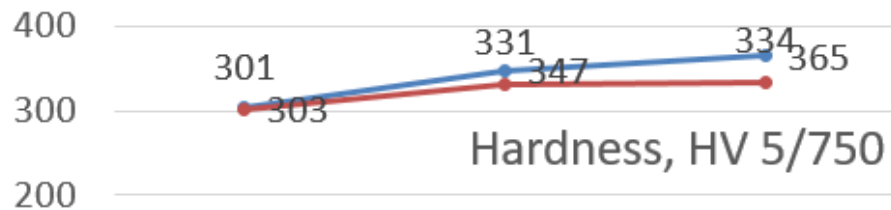
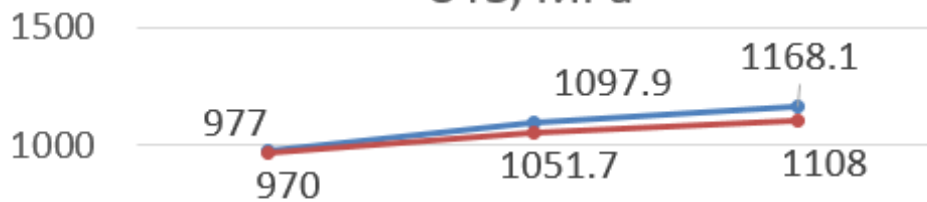


100 micrometer

Ø 30 mm. still air



### UTS, MPa

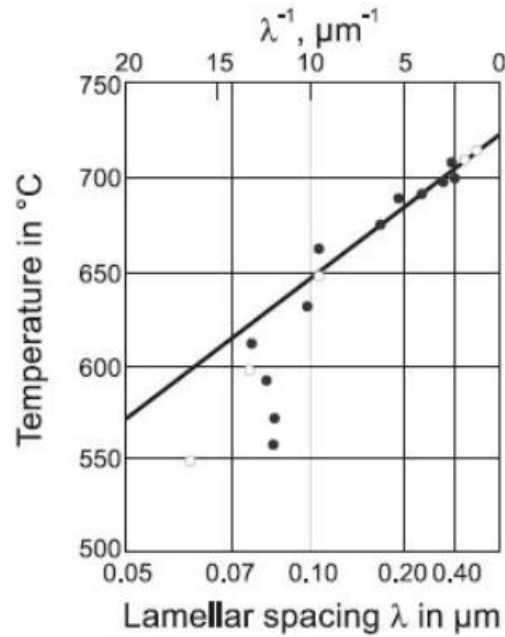
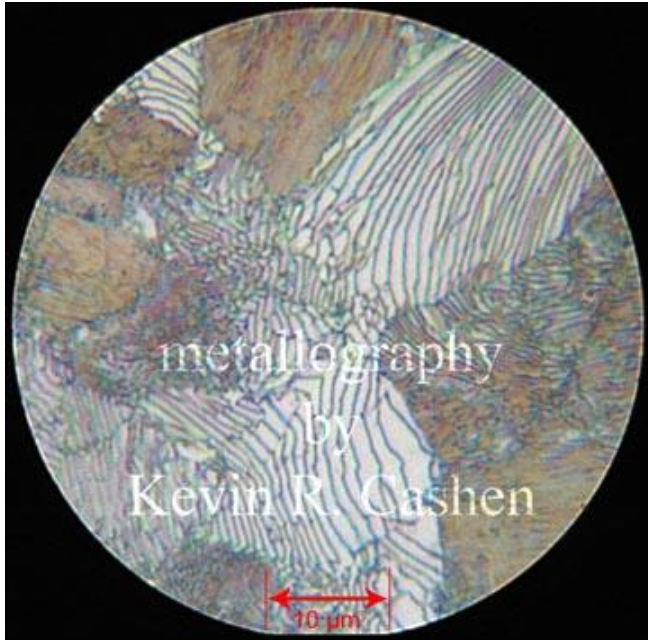


# Calculation of Strengthening Factors

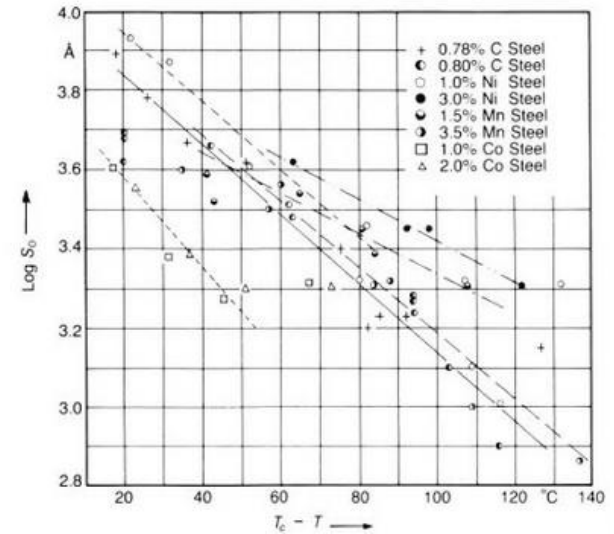
$$\begin{aligned} YS &= f_{\alpha} \{ 35 + 58(\%Mn) + 17.4(D_{\alpha})^{-0.5} \} + (1 - f_{\alpha}) \{ 178 + 3.8(\lambda_p)^{-0.5} \} \\ &+ 63(\%Si) + 425(\%N)^{-0.5} + \Delta YS_p \end{aligned}$$

Annotations: A green checkmark is above the first term, a green question mark is above the second term, a green checkmark is below the third term, and a green question mark is below the fourth term.

# Calculation of the Pearlite Interlamellar Spacing



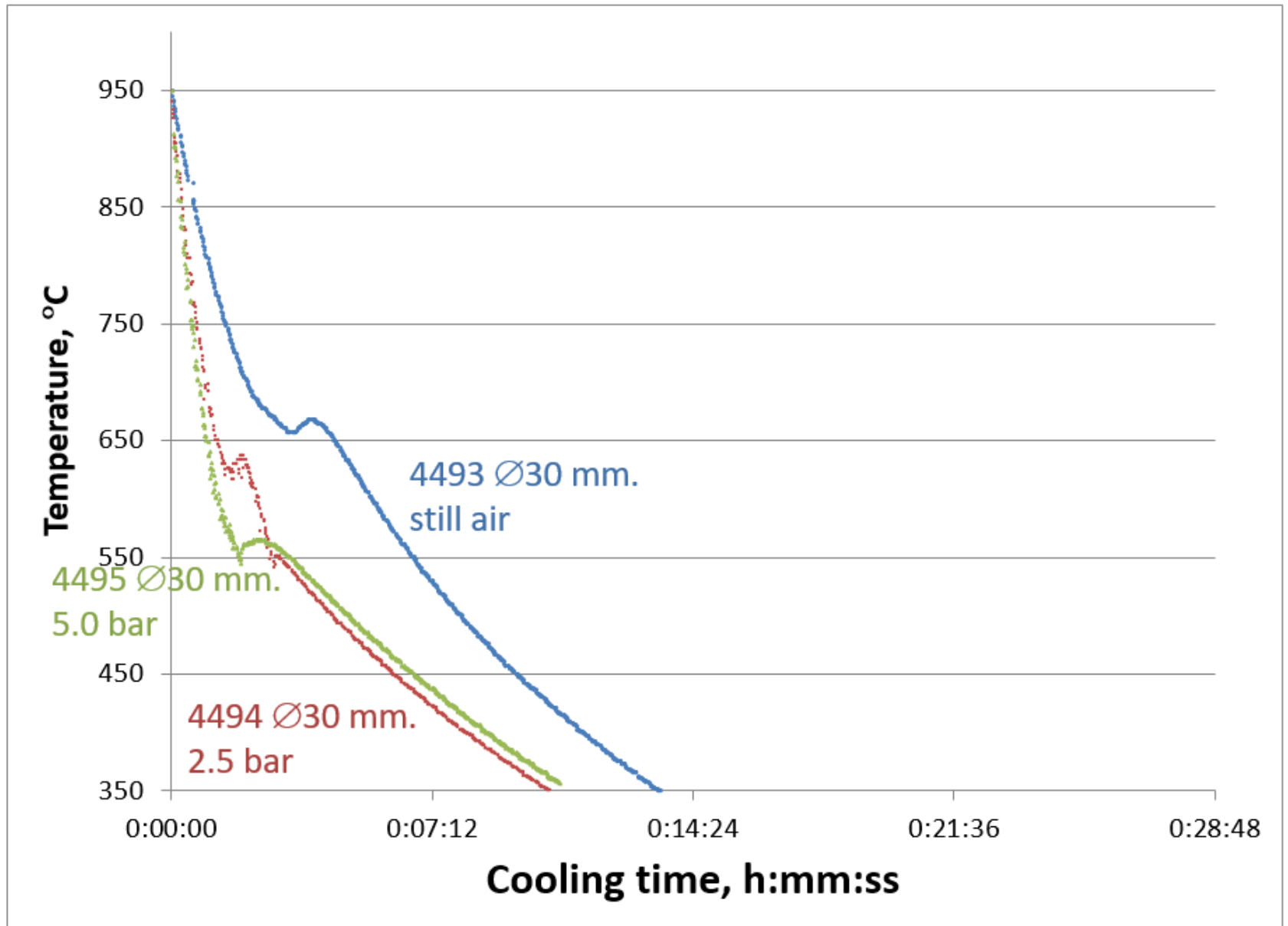
Bleck



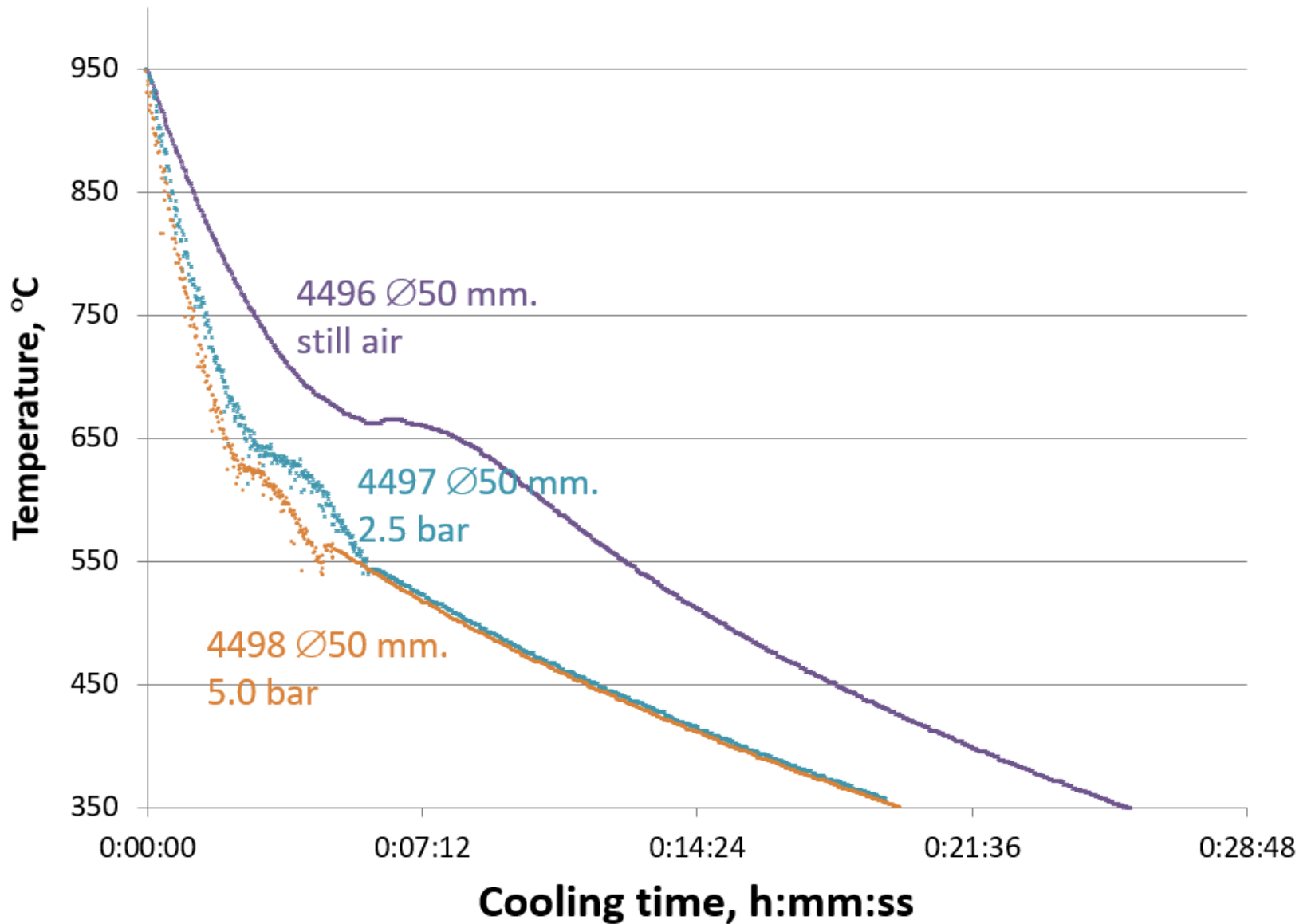
Mehl and Hagel

$$\lambda = \frac{7}{\Delta T}$$

# Results: Cooling Curves with Recalescence




# Results: Cooling Curves with Recalescence






# Calculation of the Precipitation Hardening

$$\begin{aligned}
 YS &= f_{\alpha} \{ 35 + 58(\%Mn) + 17.4(D_{\alpha})^{-0.5} \} + (1 - f_{\alpha}) \{ 178 + 3.8(\lambda_p)^{-0.5} \} + 63(\%Si) \\
 &+ 425(\%N)^{-0.5} + \Delta YS_p
 \end{aligned}$$



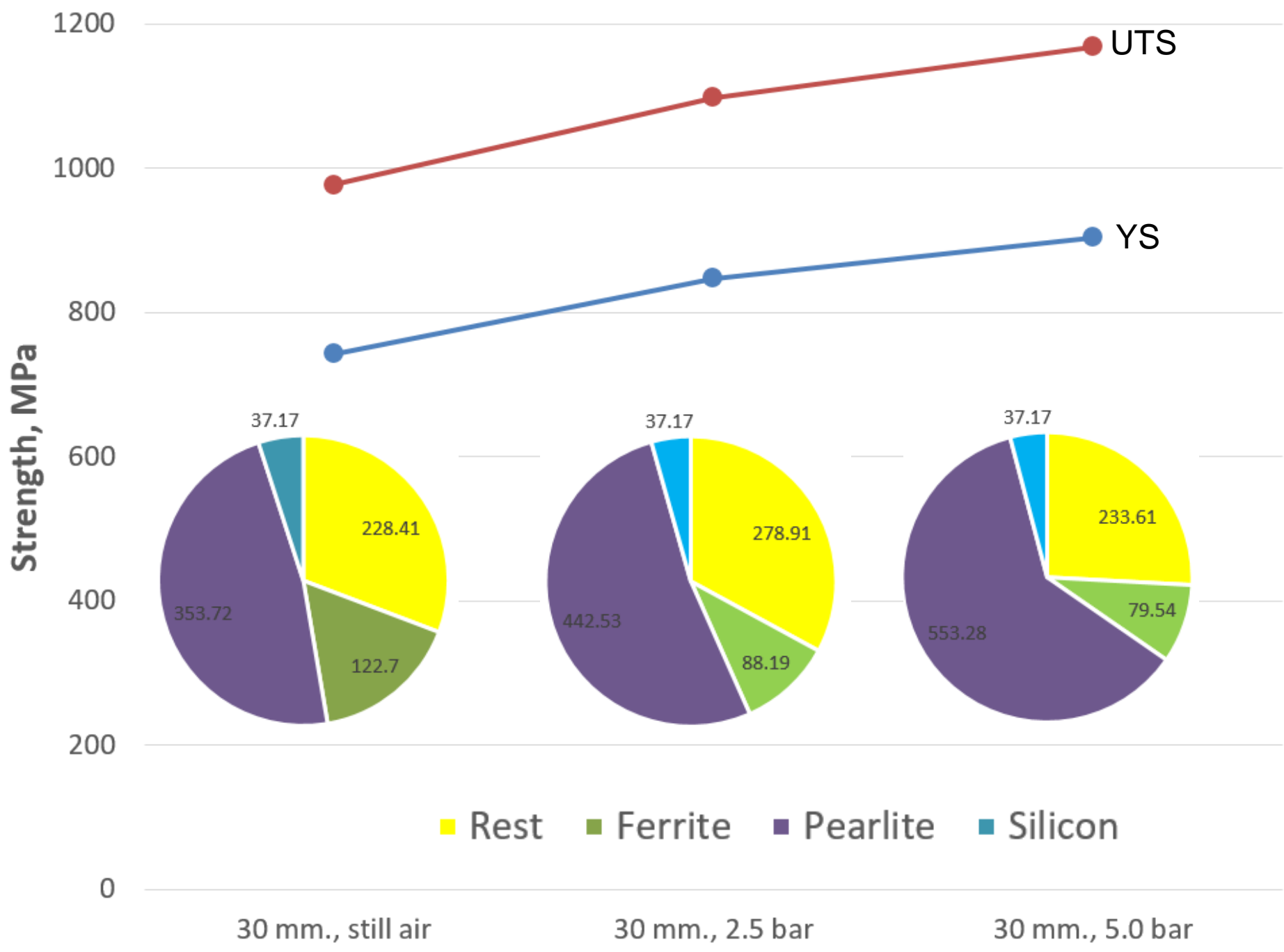


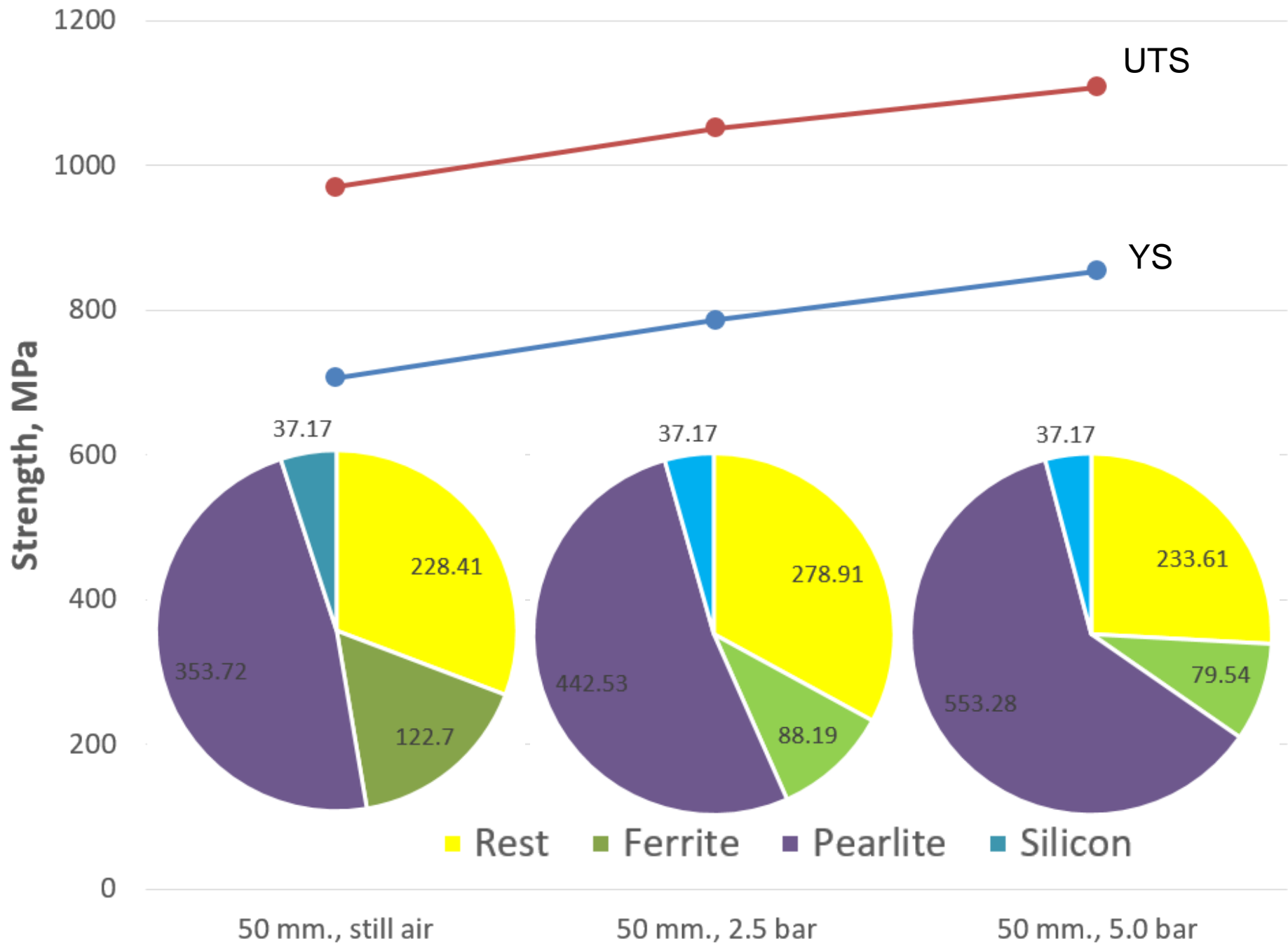


$$\Delta YS_{p,Orowan-Ashby} = \frac{0.8MGb}{2\pi\sqrt{1-\nu}L_{VC}} \ln\left(\frac{x}{2b}\right) \text{ (MPa)}$$

$$L_{VC} = \sqrt{\frac{2}{3}} \left( \sqrt{\frac{\pi}{f}} - 2 \right) r_{VC} \quad x = 2 \sqrt{\frac{2}{3}} r_{VC}$$

M – Taylor Factor, G – Shear modulus, b – Burger vector,  $\nu$  - Poison's ratio





# The 2 Unknown Strengthening Fractions

## 1. Free Nitrogen

- Too difficult (for me ;-))

## 2. Precipitation hardening

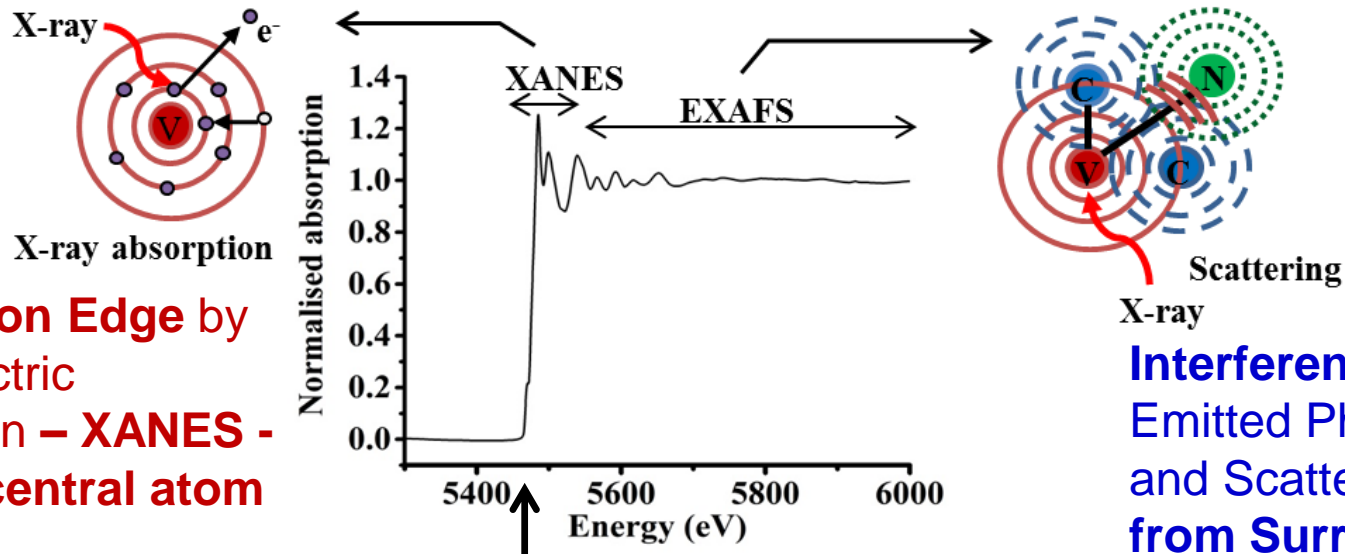
- Theoretically by measuring volume and average radius of the precipitates for the mean distance between particles

$$\begin{aligned} \Delta Y S_{p, Orowan-Ashby} \\ = \frac{0.8MGb}{2\pi\sqrt{1-\nu}L_{VC}} \ln\left(\frac{x}{2b}\right) \text{ (MPa)} \end{aligned}$$

$$L_{VC} = \sqrt{\frac{2}{3}} \left( \sqrt{\frac{\pi}{f}} - 2 \right) * r_{VC} \text{ (m)}$$

# Calculation of Precipitates Fraction vs. Dissolved Fraction

## Synchrotron XAS for the Precipitation Fraction



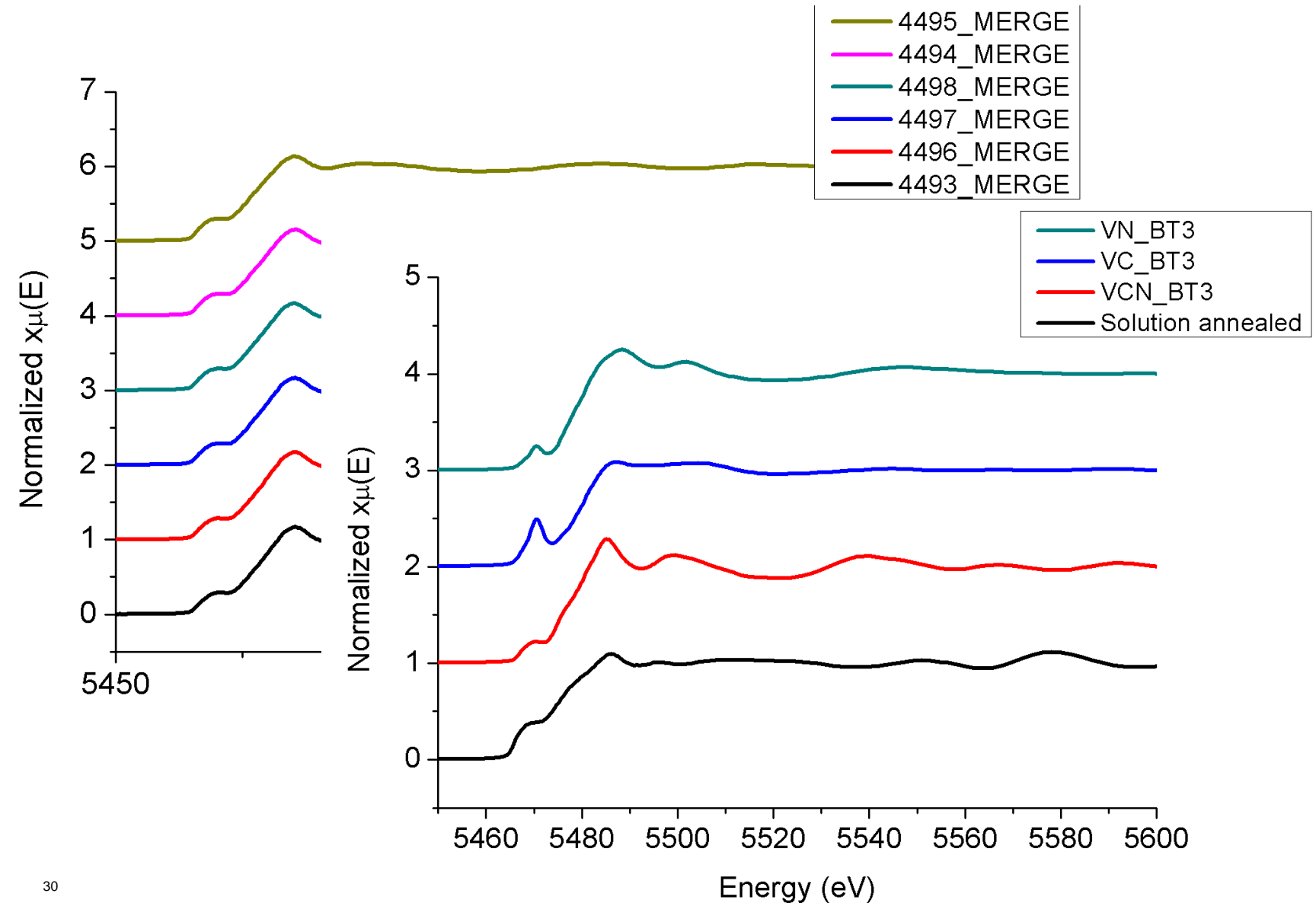
**Absorption Edge by Photoelectric Absorption – XANES – defines central atom type**

5465 eV for K-shell binding energy in V

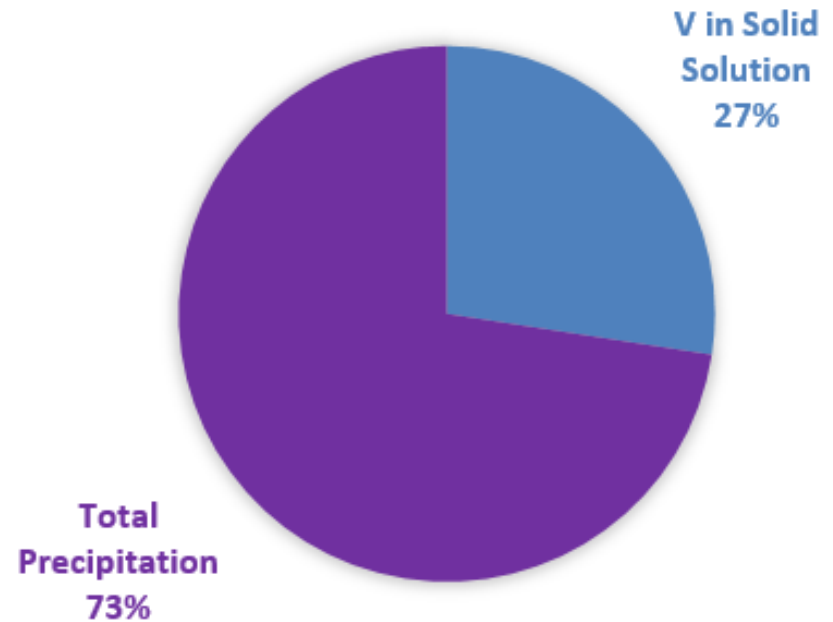
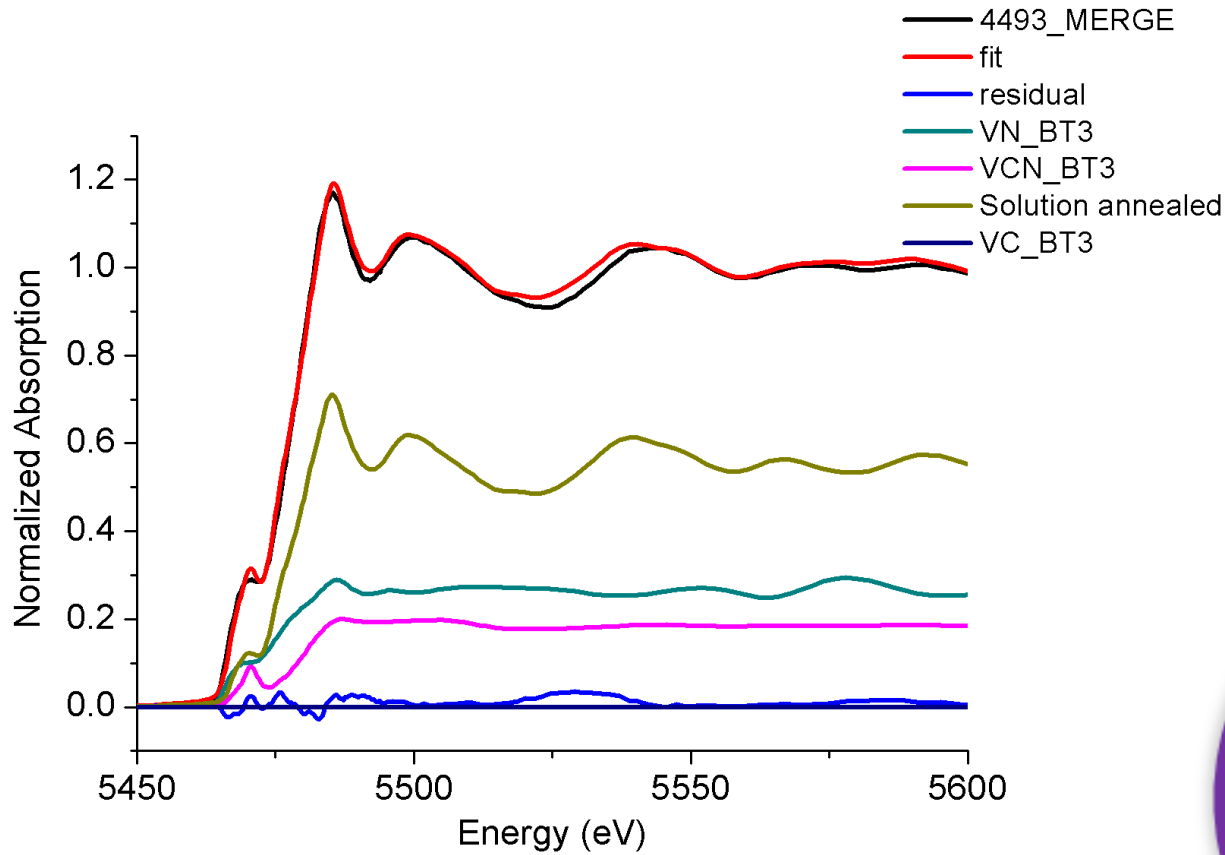
**Interference between Emitted Photoelectron and Scattered X-Ray from Surrounding Atoms – EXAFS – defines type of surrounding atoms**

$$\chi(k) = \sum_f \frac{S_0^2 N_j}{k R_j^2} |f_j^{eff}(k, R_j)| \sin[2kR_j + \varphi_j(k)] e^{-2\sigma_j^2 k^2} e^{-\frac{R_j}{\lambda(k)}}$$

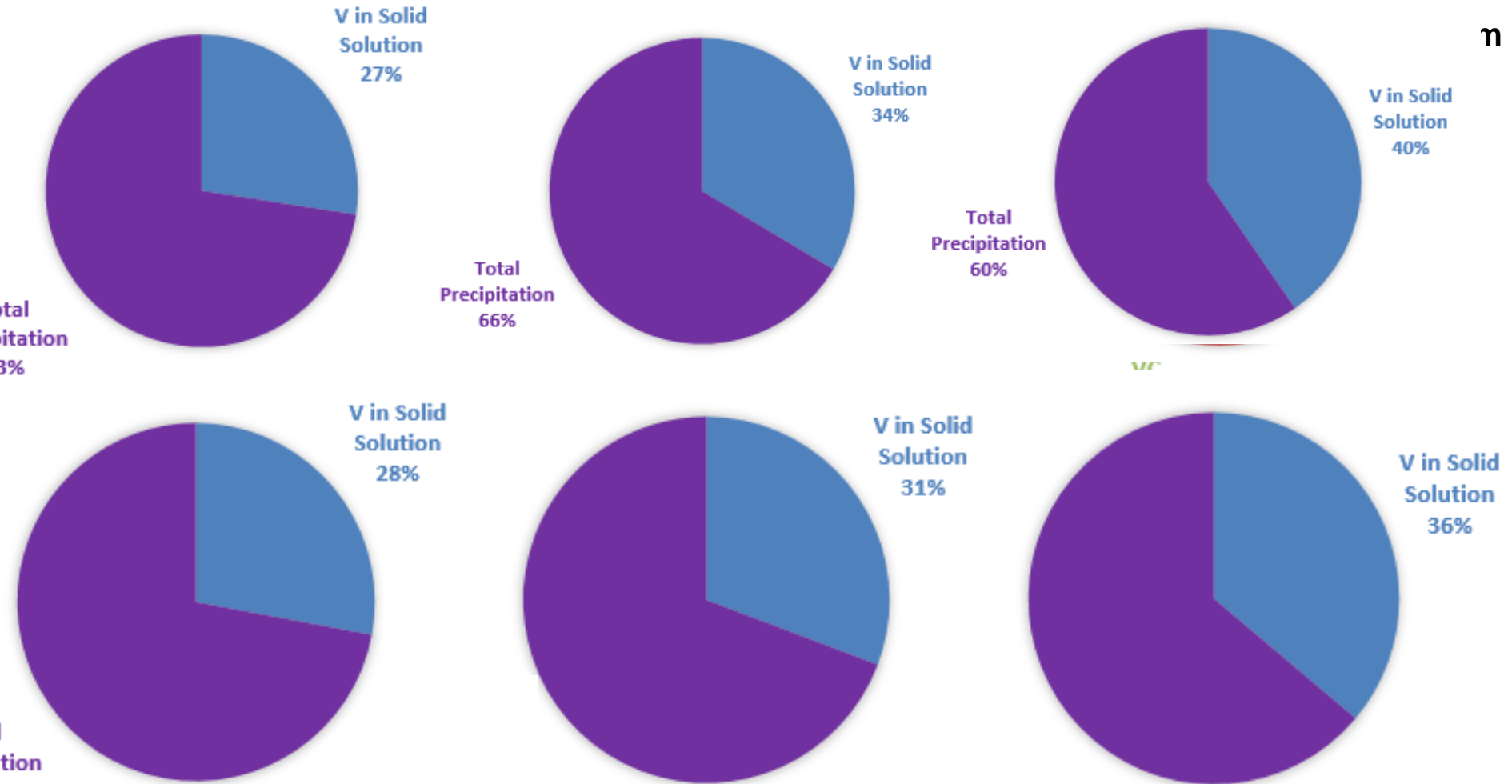
# XAS Spectra on the Samples and Standard



# Calculation of Precipitates Fraction vs. Dissolved Fraction



# Results on XAS Fractions for All Samples



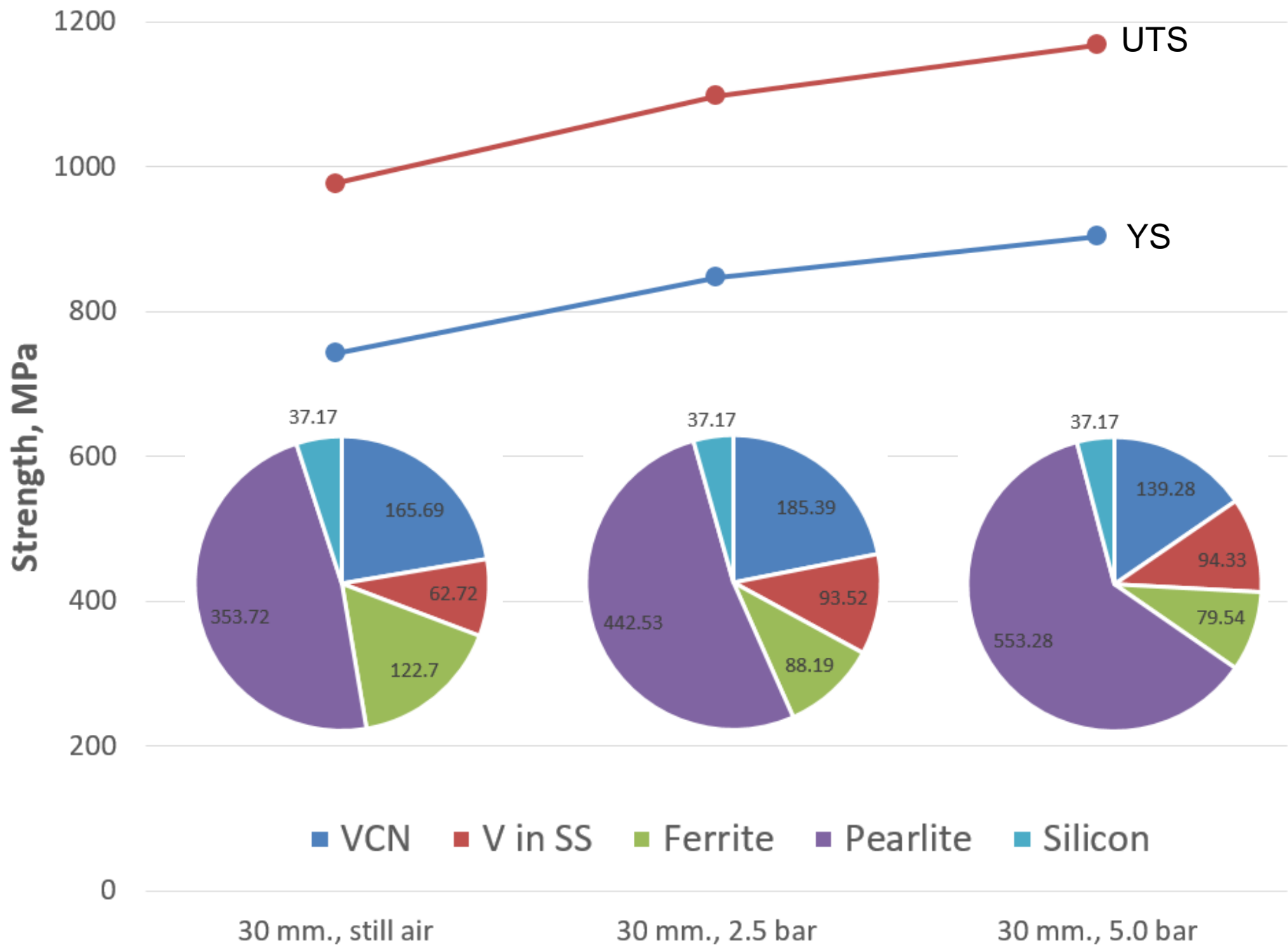


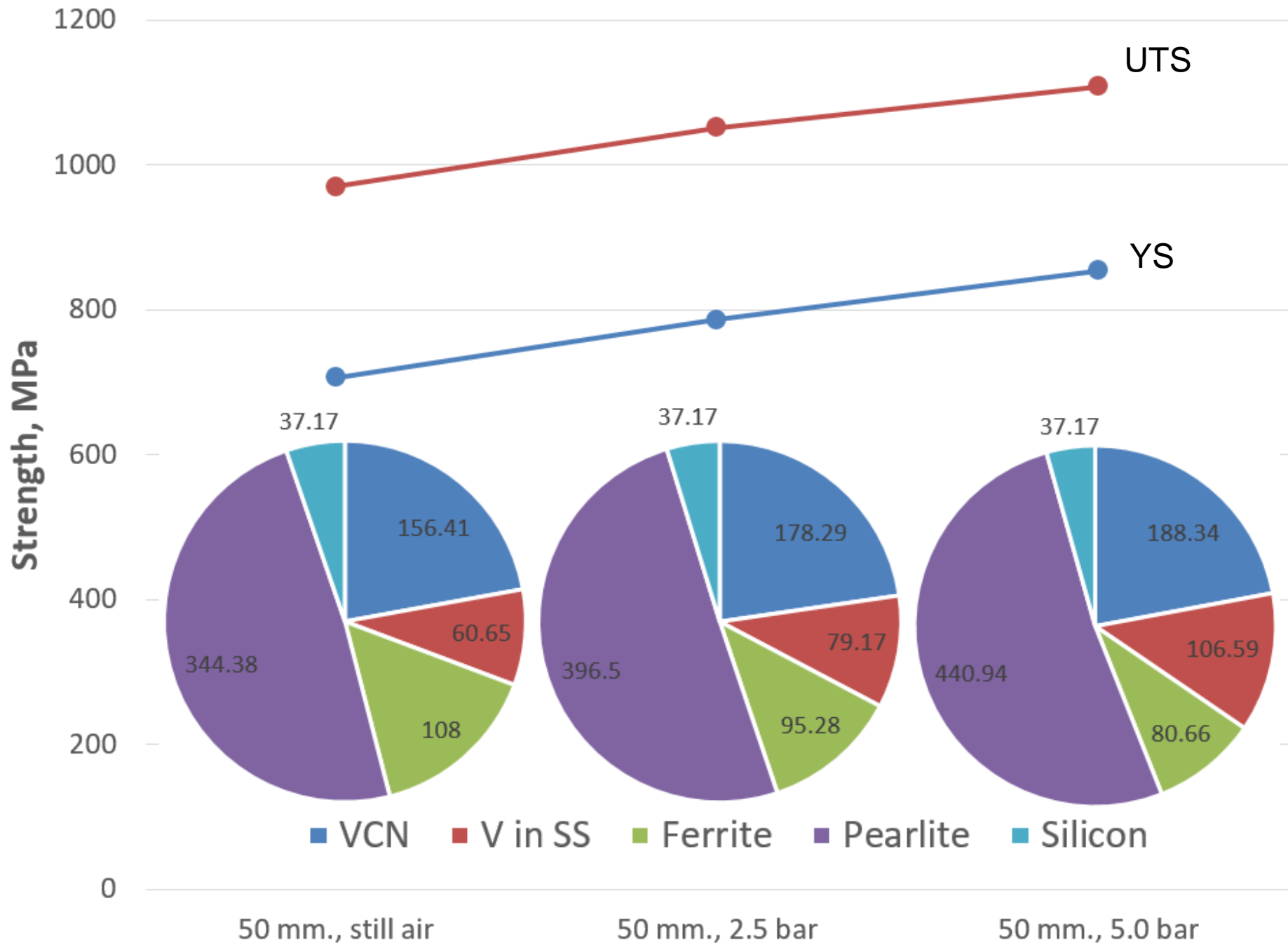
# Hooray!!! All Terms can be Solved!!!

YS

$$= f_{\alpha} \{ 35 + 58(\%Mn) + 17.4(D_{\alpha})^{-0.5} \} + (1 - f_{\alpha}) \{ 178 + 3.8(\lambda_p)^{-0.5} \} + 63(\%Si)$$
$$+ 425(\%N)^{-0.5} + \Delta YS_p$$

✓ ✓ ✓ ✓ ✓





# Conclusions

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**Forged Components can be Forged and Air Cooled Without Heat Treatment**

**Extra Ordinary Strength from Conventional Composition, mainly from Pearlite**

**Process Window for Different Bar Sizes can be Determined**

**27-40% of Vanadium is still in the Solid Solution**

**At Highest Cooling Rate (Highest Air Pressure), Lowest Fraction Contributed by Precipitation Hardening**

**6**

**The Methodology can be Followed in the Industry – Both Production and R&D**

# Acknowledgement



**GEORGSMARIENHÜTTE GMBH - [WWW.GMH-GRUPPE.DE/DE-EN/](http://WWW.GMH-GRUPPE.DE/DE-EN/)**